INITIAL SAFETY FACTOR ASSESSMENT PLANT BARRY GYPSUM STORAGE FACILITY ALABAMA POWER COMPANY

EPA's "Disposal of Coal Combustion Residuals from Electric Utilities" Final Rule (40 C.F.R. Part 257 and Part 261), §257.73(e), requires the owner or operator of an existing CCR surface impoundment to conduct periodic safety factor assessments. The owner or operator must document that the minimum safety factors outlined in §257.73(e)(1)(i) through (iv) for the critical embankment section are achieved.

The CCR surface impoundment located at Alabama Power Company's Plant Barry also referred to as the Plant Barry Gypsum Storage Facility is located on Plant Barry property, near Bucks, Alabama. The lined CCR surface impoundment is formed by an engineered perimeter embankment. The critical section of this CCR unit has been determined to be located on the west side of the unit.

The analyses used to determine the minimum safety factor for the critical section resulted in the following minimum safety factors:

Loading Condition	Minimum Calculated	Minimum Required
	Safety Factor	Safety Factor
Long-term Maximum Storage Pool (Static)	1.8	1.5
Maximum Surcharge Pool (Static)	1.7	1.4
Seismic	1.7	1.0

The embankments are constructed of well compacted clayey sands that are not susceptible to liquefaction. Therefore, a minimum liquefaction safety factor determination was not required.

I hereby certify that the safety factor assessment was conducted in accordance with 40 C.F.R. Part 257.73 (e)(1).

Jamea . Pegues, R Licensed State of Alabama, PE No. 16516 mannan



Engineering and Construction Services Calculation

Calculation Number: TV-BA-APC387586-591-002

Project/Plant:	Unit(s):	Discipline/Area:					
Plant Barry Gypsum Storage Facility	Units 1-5	ES&FS					
Title/Subject:							
Factor of Safety Assessment for CCR Rule							
Purpose/Objective:							
Analyze slope stability of Gypsum Storage Facil	ity						
System or Equipment Tag Numbers:	Originator:						
NA	Rajendra S. Gondhalekar						

Contents

Торіс	Page	Attachments (Computer Printouts, Tech. Papers, Sketches, Correspondence)	# of Pages
Purpose of Calculation	2	Attachment A – Cell 1 Construction Drawings	2
Methodology	2	Attachment B – Analysis Section Location	1
Criteria and Assumptions	3		
Summary of Conclusions	4		
Design Inputs/References	5		
Body of Calculation	5-8		
Total # of pages including cover sheet & attachments:	13		

Revision Record

Rev. No.	Description	Originator Initial / Date	Reviewer Initial / Date	Approver Initial / Date
0	Issued for Information	RSG/10-04-16	JAL/10-04-16	JCP/10-04-16

Notes:

Purpose of Calculation

Barry Steam Plant is owned and operated by Alabama Power Company and located 30 miles north of Mobile, Alabama, off of Hwy 43 near Bucks, Alabama. Plant Barry is a seven unit generating facility, including two natural gas fired combined cycle units and five coal fired units. Plant Barry is in the process has installed a flue gas desulfurization system (scrubber) on Unit 5. This process produces gypsum as a by-product. The FGD gypsum is sluiced to a lined facility for final storage or disposal.

The gypsum storage facility will be constructed in a four cell arrangement with construction of Cell 1 currently completed. Additional cells will be completed as capacity demands dictate. Construction of the Cell 1 involved grading of the existing ground surface and the constructing of a perimeter dike out of compacted fill. The inside of Cell 1 was be lined with a high-density polyethylene (HDPE) liner to prevent infiltration of decant water into the subsurface. A drainage system utilizing a layer of geogrid sandwiched between layers of geofabric (i.e. TexDrain) carries decant water from the bottom of the cell to collection pipes which discharge into a sediment basin. A plan view of the Cell 1 design is shown in the Attachments.

The perimeter dike has been constructed using compacted fill from a nearby borrow area. This fill consists of silty and clayey sands. The dike averages approximately 20 feet in height and will varies in top width from 16 to 32 feet. The top of the dike at the critical section is at approximately elevation EL31 based on the latest topographic map. The exterior slope of the dikes is at 3H:1V and the interior slope of dikes within Cell 1 is at 2H:1V.

During operation, gypsum slurry is sluiced into the cell and allowed to decant through the drainage system. The dry gypsum that remains is used to create perimeter dikes, allowing the sluiced gypsum to be raised in levels to a final height of approximately 77 feet. A 3H:1V exterior slope will be maintained for the gypsum, and a 16 foot set-back will be constructed between the gypsum levels. Cross-sections showing the levels of gypsum placement in Cell 1 are shown in the Attachments.

The purpose of this calculation is to evaluate the stability of Plant Barry's gypsum storage facility and dike at the critical analysis section located on the after the final level of gypsum placement in Cell 1.

Methodology

The calculation was performed using the following methods and software:

GeoStudio 2012 (Version 8.15, Build 11777), Copyright 1991-2016, GEO-SLOPE International, Ltd.

Strata (Version alpha, Revision 0.2.0), Geotechnical Engineering Center, Department of Civil, Architectural, and Environmental Engineering, University of Texas.

Morgenstern-Price analytical method was run and reported.

Criteria and Assumptions

The slope stability models were run using the following assumptions and design criteria:

- Seismic site response was determined using a one-dimensional equivalent linear site response analysis. The analysis was performed using Strata, utilizing random vibration theory. The input motion consisted of the USGS published 2008 Uniform Hazard Response Spectrum (UHRS) for Site Class B/C at a 2% Probability of Exceedance in 50 years. The UHRS was converted to a Fourier Amplitude Spectrum, and propagated through a representative one dimensional soil column using linear wave propagation with strain-dependent dynamic soil properties. The input soil properties and layer thickness were randomized based on defined statistical distributions to perform Monte Carlo simulations for 100 realizations, which were used to generate a median estimate of the surface ground motions.
- The median surface ground motions were then used to calculate a pseudostatic seismic coefficient for utilization in the stability analysis using the approach suggested by Bray and Tavasarou (2009). The procedure calculates the seismic coefficient for an allowable seismic displacement and a probability exceedance of the displacement. For this analysis, an allowable displacement of 0.5 ft, and a probability of exceedance of 16% were conservatively selected, providing a seismic coefficient of 0.008g for use as a horizontal acceleration in the stability analysis.
- The current required minimum criteria (factors of safety) were taken from the Structural Integrity Criteria for existing CCR surface impoundment from 40 CFR 257.73, published April 17, 2015.
- The soil properties of unit weight, phi angle, and cohesion were obtained from historical laboratory and in-situ test results.
- Soil stratigraphy and piezometric data was estimated from the historical boring logs.
- The properties of unit weight, phi angle, and cohesion for the gypsum were derived from laboratory test data from Plant Scholz gypsum samples including the following: sedimented consolidation samples, cast and sedimented triaxial samples, cast gypsum samples, and in-situ tests on sedimented gypsum
- The COE EM 1110-2-1902, October 2003, allows the use of the phreatic surface established for the maximum storage condition (normal pool) in the analysis for the maximum surcharge loading condition. This is based on the short term duration of the surcharge loading relative to the permeability of the embankment and the foundation materials. This method is used in the analysis for the impoundments at this facility with surcharge loading.

The Cross-Section and materials used in this survey calculation were generally gathered from historical slope stability analyses for the gypsum storage facility. The critical section for the storage facility was identified to be located along the west side of Cell 1.

Input Data

The following soil properties were used in the analyses.

Soil Type	Unit Weight,	Cohesion,	Phi Angle,
	pcf	psf	deg
Gypsum	85	0	30
Dike Fill	122	500	26
Base Soil	110	300	20

Hydrologic Considerations

Since the analysis condition consists of the gypsum stack being at a significantly higher elevation than the perimeter dikes and drainage channels, the gypsum will not receive any runoff from the surrounding areas. For the purpose of the analyses, the hydrologic conditions in the gypsum stack were conservatively assumed to be at the operating pool elevation for the previous level for the long term maximum storage condition, and at the surface of the gypsum top deck for the maximum surcharge condition.

Load Conditions

The stability of the Plant Barry gypsum storage facility was evaluated for the load conditions indicated in the following table. When appropriate, cases were run both in the gypsum and the dike.

Summary of Conclusions

The following table lists the factors of safety for various slope stability failure conditions. All conditions are steady state except where noted. Construction cases were not considered. Based on the results of these analyses all structures are stable.

North East Main Dike												
Case	Computed Factor of Safety	Typical Minimum Factor of Safety										
Long-term Maximum Storage Pool (Static)	1.8	1.5										
Maximum Surcharge Pool (Static)	1.7	1.4										
Seismic	1.7	1.0										

The analyses indicate that in all cases, the factors of safety are above the required minimums.

Design Inputs/References

- USGS Earthquake Hazards website, <u>http://www.usgs.gov/hazards/earthquakes/</u>.
- US Corps of Engineers Manual EM 1110-2-1902, October 2003
- Bray, J. D. and Travasarou, T., *Pseudostatic Coefficient for Use in Simplified Seismic Slope Stability Evaluation*, Journal of Geotechnical and Environmental Engineering, American Society of Civil Engineers, September 2009

Body of Calculation

Calculation consists of Slope-W modeling attached.













Attachment A

Figure – Cell 1 Construction Drawings



	(IN	FE	ET)
1	ir	nch	=	50	ft

																																This docun of The South authorized co use, distrib	Copyright [©] Soment contains ern Company ntractors of, ution, copying	Southern C puthern Compa proprietary, cor or of third par the subsidiaries dissemination,	ompany Servi ny Services, fidential, and, ies. It is inte of the South or disclosure	ces, Inc. nc. All Righ [.] for trade secr nded for use ern Company. of any portic	s Reserved et information only by empl Unauthorized n hereof is
DATE	-80	-14-09		RE∨ISI	ON 4		DA	ΓE 0 ⁻	7–02–09		RE∨ISI	.ON 3		DATE	03-0	5–09	٦	REVISION	2		DAT	<u> </u>	-14-08		RE∨IS	ION 1		DAT	E 04-	-11-08		RE∨ISI	IN	0	DATI	-	12-03-0
.9				A. C-4,	F-7 Al	DDED GUA	RDRAIL AI	ND SWING	GATE		A. G-7	ADDED	PIPE SLEE	EVES AND P	PIPING		IS	ISSUED FOR CONSTRUCTION ISSUED FOR CONSTRUCTION										ISSUED FOR CONSTRUCTION									
JTH EV	ACUATIO	N NOTE.									B. H-7	ADDED	ELECT DU	CT RUN			G	ENERAL RE	VISION						GENERA	L REVISION	١										
с то о	с'-с'										С. В-6	ADDED	ELECT DU	CT RUN																							
CL											D. F-7	ADDED	ELECT DU	CT RUN ANI	D EDITED I	NOTE																					
ET STAC	CKING A	REA EWO	2161DE						EWC) 2161DE	E. F-8	ADDED	PIPE SLEE	EVE AND PIF	PING	EWO 216	1DE						EWO	2161DE						EWO	2161DE						EWO
APPR I.	/C APPR	MECH APPR	DISC MGR	BY	СНК′Д	CIVIL APPR	RELECT APP	R I/C APPR	MECH APPR	DISC MGR	BY	СНК′Д	CI∨IL APPR	ELECT APPR I	C APPR ME	CH APPR DISC	MGR	BY C	нк′д сі∨	VIL APPR E	LECT APPR	I/C APPR	MECH APPR	DISC MGR	BY	СНК′Д	CIVIL APPF	RELECT APPR	I/C APPR	MECH APPR	DISC MGR	BY	СНК′Д	CI∨IL APPR	ELECT APPR	I/C APPR	MECH APPR
м	KAH	TDJ	СКТ	JWM	PMG	BRH	JTM	KAH	TDJ	СКТ	JWM	PMG	BRH	JTM	КАН	тој ск	т	JWM P	MG	BRH	JTM	KAH	TDJ	СКТ	JWM	PMG	BRH	JTM	КАН	RAM	СКТ	JWM	PMG	BRH	JTM	KAH	RAM
					1		1		1			1											1	1					1	1							

ANSI E: 44×34



			3			۲ ۲
	GYPSUM SLUICE L)) ご INES TO BE				
14	SLOPES TO LEVEL	E GYPSUM DIKE 2 AND LEVEL 3				
20		SLUICE I	LINES AND DITCH			
25					· · · · · · · · · · · · · · · · · · · ·	
30	30 30 30	DIKE EL. 31.00		A Cost	Åuuu	min
	30			E C		
	35	31.00				
	40 45				sting	
Â			16'			
	55-7 51.40).27%			CELL 1-STORAGE CAP
	265 70		3:1			INCOMING FLOW RATE GYPSUM PRODUCTION
P	72 71.90					FINAL CELL 1 STACK STORAGE VOLUME CAP OR 1,380,565,620 LE
						STORAGE LIFE - 5.96 DESIGN OF CELL BAS
		- 40 50	-25	20 25 30 4	~	INCOMING FLOW RATE GYPSUM PRODUCTION
	70 72			T0P 0		FINAL CELL 1 STACK STORAGE VOLUME CAP OR 1.380,565,620 LE
		25'	20'	FDIKE	S	DESIGN OF CELL BAS
75	3:	3:	:1	EL. 3		INCOMING FLOW RATE GYPSUM PRODUCTION
NO.			3:1	-1. 00 2:1	B	FINAL CELL 1 STACK STORAGE VOLUME CAP OR 1.380.565.620 LE
PPROX 18.	61 ACRES					STORAGE LIFE - 1.41
TIONS THIS	SHEET)					
L XCC						
		FOR TYPIC	CAL RAMP			(FL
	4.00%	E5C11050		16' 		
8 72					A CON	
TOPE	EL. 77±	100 100 100 100 100 100				
5C110			SIPHON SHOWN E LEVEL 2. AFTER 2 FILLING, SIPHON S	XTENDED TO 2ND LEVEL SHALL BE		
		11050	REMOVED. SEE SH E5C11051 FOR DI	IEET ETAILS.		
	71.907	C0 E2 C	FIRST LEVEL	SIPHON	3:1	
		8 45'	SHALL BE RI	EMOVED AFTER		RISER AS
					20	
		51.40	40			EXTEND FUTURE CONSTRU
45				3:1		
			31.00	RIS OU COI	ER STRUCTURE AND TFALL PIPE TO BE NCRETE GROUTED,	
				IN OPI	PPED, AND ABANDONI PLACE AFTER SIPHON ERATIONS BEGIN.	
10%	25 0.1	0%0.10%		0.27%		
		0%/~				
50					A-P	
	SEE DISCH	אר אין				
				2		
	DIMENTATIO	N POND B	OTT. EL. 9.	0 =		
		r -	- 4	ty		

															Southern C uthern Compo proprietary, co or of third pa he subsidiaries dissemination	Company Serv any Services, nfidential, and rties. It is int is of the Soutl , or disclosur	ices, Inc. Inc. All Righ I/or trade sec ended for use hern Company e of any porti	nts Reserved ret information only by empl Unauthorized on hereof is p	ו סי סר
		DAT	E			REVISI	I NC		DAT	DATE 09-04-09				0 NC		DAT	E 12	-31-08	
						GENERAL	REVISION						ISSUED	FOR CONS	TRUCTION				
											EWO	2161DE						EWO	
CHK'D	CIVIL APPR	ELECT APPR	I/C APPR	MECH APPR	DISC MGR	BY	СНК'Д	CIVIL APPR	ELECT APPR	I/C APPR	MECH APPR	DISC MGR	BY	СНК′Д	CIVIL APPR	ELECT APPR	I/C APPR	MECH APPR	
						EEJ	PMG	BRH	JTM	KAH	TDJ	СКТ	JWM	PMG	BRH	JTM	КАН	TDJ	

ANSI E: 44×34

Acad2004

Attachment B

Figure – Analysis Section Location

